

APPENDIX D

PRISMATIC COMPRESSION OF LENGTH BARS

(These results were derived by mathematicians in NPL's Division of Information Technology and Computing).

With reference to Timoshenko & Goodier [1], the forces in the body are

$$X = Y = 0, \quad Z = -\rho g$$

The differential equations of equilibrium ((127) of Timoshenko & Goodier) are satisfied by

$$\sigma_z = \rho g(z - l), \quad \sigma_x = \sigma_y = \tau_{xy} = \tau_{yz} = \tau_{xz} = 0$$

i.e. by assuming that on each cross section we have a uniform compression produced by the upper portion of the bar (see figure D.1).

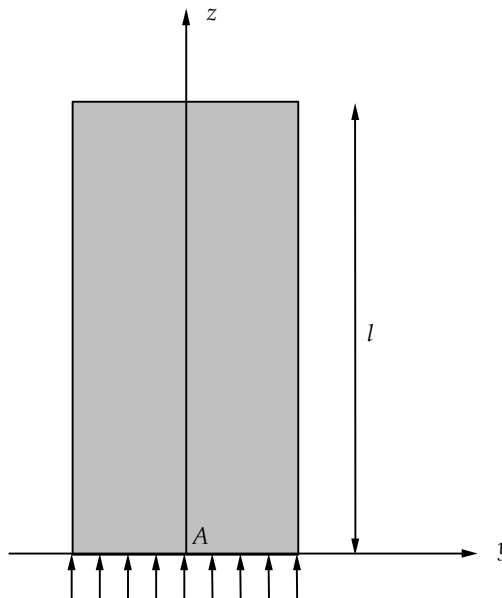


Figure D.1 - Compression on cross section of bar

Hooke's law gives

$$\varepsilon_z = \frac{\partial w}{\partial z} = \frac{\sigma_z}{E} = \frac{\rho g}{E}(z - l) \quad (\text{D.1})$$

$$\varepsilon_x = \varepsilon_y = \frac{\partial u}{\partial x} = \frac{\partial v}{\partial y} = -\nu \frac{\rho g}{E} (z-l) \quad (\text{D.2})$$

$$\gamma_{xy} = \gamma_{xz} = \gamma_{yz} = \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} = \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} = \frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} = 0 \quad (\text{D.3})$$

Integrating (D.1) gives

$$w = \frac{\rho g z^2}{2E} - \frac{\rho g l z}{E} + w_0 \quad (\text{D.4})$$

where w_0 does not depend on z , i.e. $w_0 = w_0(x,y)$. Substituting (D.4) into the second and third of equations (D.3) we find

$$\frac{\partial w_0}{\partial x} + \frac{\partial u}{\partial z} = 0, \quad \frac{\partial w_0}{\partial y} + \frac{\partial v}{\partial z} = 0$$

from which

$$u = -z \frac{\partial w_0}{\partial x} + u_0, \quad v = -z \frac{\partial w_0}{\partial y} + v_0 \quad (\text{D.5})$$

where u_0 and v_0 are functions of x and y only. Substituting these expressions into (D.2) we find

$$-z \frac{\partial^2 w_0}{\partial x^2} + \frac{\partial u_0}{\partial x} = -\frac{\nu \rho g}{E} (z-l), \quad -z \frac{\partial^2 w_0}{\partial y^2} + \frac{\partial v_0}{\partial y} = -\frac{\nu \rho g}{E} (z-l)$$

Equating polynomial terms in z , we have

$$\frac{\partial^2 w_0}{\partial x^2} = \frac{\partial^2 w_0}{\partial y^2} = \frac{\nu \rho g}{E}, \quad \frac{\partial u_0}{\partial x} = \frac{\partial v_0}{\partial y} = \frac{\nu \rho g l}{E} \quad (\text{D.6})$$

Substituting expressions (D.5) into the first of equations (D.3), we find

$$-2z \frac{\partial^2 w_0}{\partial x \partial y} + \frac{\partial u_0}{\partial y} + \frac{\partial v_0}{\partial x} = 0$$

and since u_0 and v_0 do not depend on z , we have

$$\frac{\partial^2 w_0}{\partial x \partial y} = 0, \quad \frac{\partial u_0}{\partial y} + \frac{\partial v_0}{\partial x} = 0 \quad (\text{D.7})$$

From the six equations in (D.6) and (D.7) we can write general expressions for u_0 , v_0 and w_0 . All these equations are satisfied by

$$u_0 = \frac{\nu \rho g l x}{E} + \delta y + \delta_1$$

$$v_0 = \frac{\nu \rho g l y}{E} - \delta x + \gamma_1$$

$$w_0 = \frac{\nu \rho g}{2E} (x^2 + y^2) + \alpha x + \beta y + \gamma$$

Now substituting these expressions into equations (D.4) and (D.5), the general expressions for the displacements are

$$u = -\frac{\nu \rho g x z}{E} - \alpha z + \frac{\nu \rho g l x}{E} + \delta y + \delta_1$$

$$v = -\frac{\nu \rho g y z}{E} - \beta z + \frac{\nu \rho g l y}{E} - \delta x + \gamma_1$$

$$w = \frac{\rho g z^2}{2E} - \frac{\rho g l z}{E} + \frac{\nu \rho g}{2E} (x^2 + y^2) + \alpha x + \beta y + \gamma$$

The six arbitrary constants are determined from the conditions at the support. We prevent translatory movement of the bar by fixing the centroid A of the lower end of the bar so that for $x = y = z = 0$, we have $u = v = w = 0$. We eliminate rotation of the bar about axes through A parallel to the x and y axes by fixing an element of the z axis at A . Then $\partial u / \partial z = \partial v / \partial z = 0$ at A . We avoid the possibility of rotation about the z axis by ensuring that $\partial v / \partial x = 0$ at the point A . From these six conditions at A , we find that all the arbitrary constants (α , β , γ , γ_1 and δ_1) vanish. Thus we are left with

$$u = \frac{\nu \rho g x}{E} (l - z)$$

$$v = \frac{\nu \rho g y}{E} (l - z)$$

$$w = \frac{\rho g z^2}{2E} + \frac{\nu \rho g}{2E} (x^2 + y^2) - \frac{\rho g l z}{E}$$

Hence for the point $(x,y,z) = (0,0,l)$ initially, we have, after deformation:

$$z = l + w(0,0,l) = l - \frac{\rho g l^2}{2E}$$

Hence the change in length of a bar when standing vertically, due to its own weight, is given by

$$-\frac{\rho g l^2}{2E}$$

Using this equation and average values for steel of $\rho = 7800 \text{ kg m}^{-3}$, $E = 208 \text{ GPa}$, $g = 9.8 \text{ m s}^{-1}$ produces the graph shown in figure D.2.

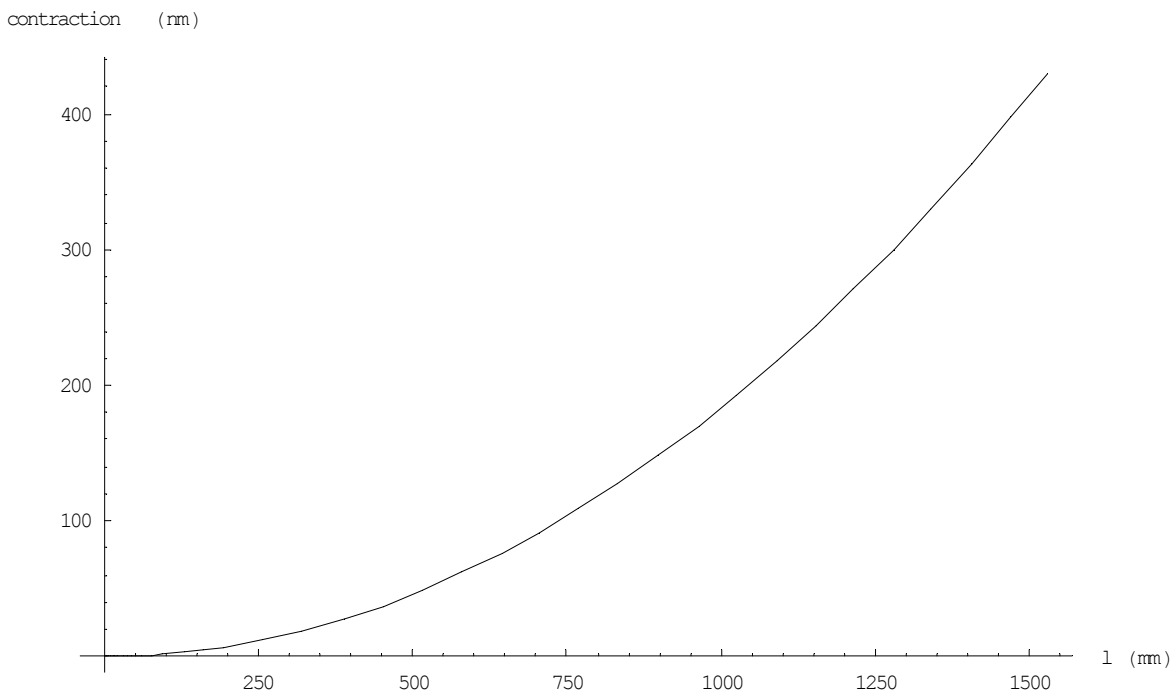


Figure D.2 - Contraction of a steel length bar, standing vertically

REFERENCES FOR APPENDIX D

- [1] Timoshenko S & Goodier J N *Theory of Elasticity* (McGraw-Hill, New York) (1951) 246